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NAVY UNDERWATER SOUND LAB NEW LONDON CONN THE OUTPUT OF A TRUE CORRELATOR WITH NOISY INPUTS. (U) SEP 66 E S EBY USL-TM-2242-244-66

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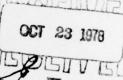
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THE OUTPUT OF A TRUE CORRELATOR WITH NOISY INPUTS

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Consider the true correlator of the figure with noisy inputs:

$$r_1(t) = s(t) + n_1(t)$$
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 $r_2(t) = s(t) + n_2(t)$

where s(t) is a signal common to both inputs and $n_1(t)$, $n_2(t)$ are noise waveforms.

> $r_1(t) = s(t) + n_1(t)$ $r_2(t) = s(t) + n_2(t)$ True Correlator Figure

The output of the correlator is

(1)
$$\rho(z) = \frac{\int_{\infty}^{\infty} r_1(t) r_2(t+z) dt}{\left[\int_{\infty}^{\infty} r_1^2(t) dt \int_{\infty}^{\infty} r_2^2(t) dt\right]^{\frac{1}{2}}}$$

Assume the signal is not correlated with either noise and let

$$S = \int_{-\infty}^{\infty} s^{2}(t) dt = signal power$$

$$N_{i} = \int_{-\infty}^{\infty} n_{i}^{2}(t) dt = i^{th} \text{ noise power, } i = 1,2$$

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Then
(2)
$$\rho(t) = \frac{\int_{0}^{\infty} (s(T) + n_{1}(T)) (s(t+T) + n_{2}(t+T)) dT}{\left[\int_{0}^{\infty} (s(t) + n_{1}(t))^{2} dt \int_{0}^{\infty} (s(t) + n_{1}(t))^{2} dt\right]^{\frac{1}{2}}}$$

Evaluation of the integrals gives

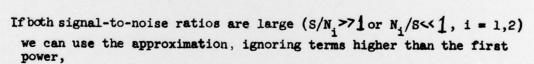
(3)
$$\rho(t) = \frac{s \rho_{ss}(t) + (N_1 N_2)^{\frac{1}{2}} \rho_{n_1 n_2}(t)}{\left[(s+N_1) (s+N_2) \right]^{\frac{1}{2}}}$$

which we can write as

(4)
$$\rho(t) = \frac{(s/N_1)^{\frac{1}{2}} (s/N_2)^{\frac{1}{2}} (p_{ss}(t) + p_{n_1n_2}(t))}{[(1 + s/N_1) (1 + s/N_2)]^{\frac{1}{2}}}$$

or

(5)
$$P(t) = \frac{\left(s_{s}(t) + (N_{1}/s)^{\frac{1}{2}} (N_{2}/s)^{\frac{1}{2}} P_{1} n_{2}(t) \right)}{\left[(1 + N_{1}/s) (1 + N_{2}/s) \right]^{\frac{1}{2}}} .$$



(6)
$$\rho(t) \approx \left[1-\frac{1}{2}(N_1/S + N_2/S)\right] \rho_{ss}(t) + (N_1/S)^{\frac{1}{2}} (N_2/S)^{\frac{1}{2}} n_1 n_2(t),$$
 if both signal-to-noise ratios are small (S/N₁<<1, i = 1,2), then the approximation becomes

(8)
$$\rho(t) = \frac{(s/N_2)^{\frac{1}{2}} \rho_{ss}(t) + (N_1/s)^{\frac{1}{2}} \rho_{n_1 n_2}(t)}{\left[(1 + N_1/s) (1 + s/N_2) \right]^{\frac{1}{2}}}$$

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give the approximation, ignoring powers higher than the first,

(9)
$$f(t) \approx (s/n_2)^{\frac{1}{2}} f_{ss}(t) + (n_1/s)^{\frac{1}{2}} f_{n_1 n_2}(t)$$
.

Hence, for high signal-to-noise ratios, the correlator output $\mathcal{C}(\mathcal{T})$ approximates the signal autocorrelation $\mathcal{C}_{ss}(\mathcal{T})$, for low signal-to-noise ratios $\mathcal{C}(\mathcal{T})$ follows the noise correlation $\mathcal{C}_{n_1n_2}(\mathcal{T})$, and in the mixed case, the correlator output is mixed. In fact, if both signal-to-noise ratios are unity (Odb), the true correlator output is just the arithmetic mean of the signal and noise correlations

(10)
$$P(t) = \frac{P_{ss}(t) + P_{1}n_{2}(t)}{2}$$
.

From the above calculation, we see that the correlator output will decrease in amplitude in the presence of noise, even if the noise cross-correlation is zero. If the noise correlation does not vanish, then this will appear as a bias on the true correlator output.